

# 1 Revue of the FEM

FEM provides formalism for generating discrete (finite) algorithms for approximating the solutions of differential equations.

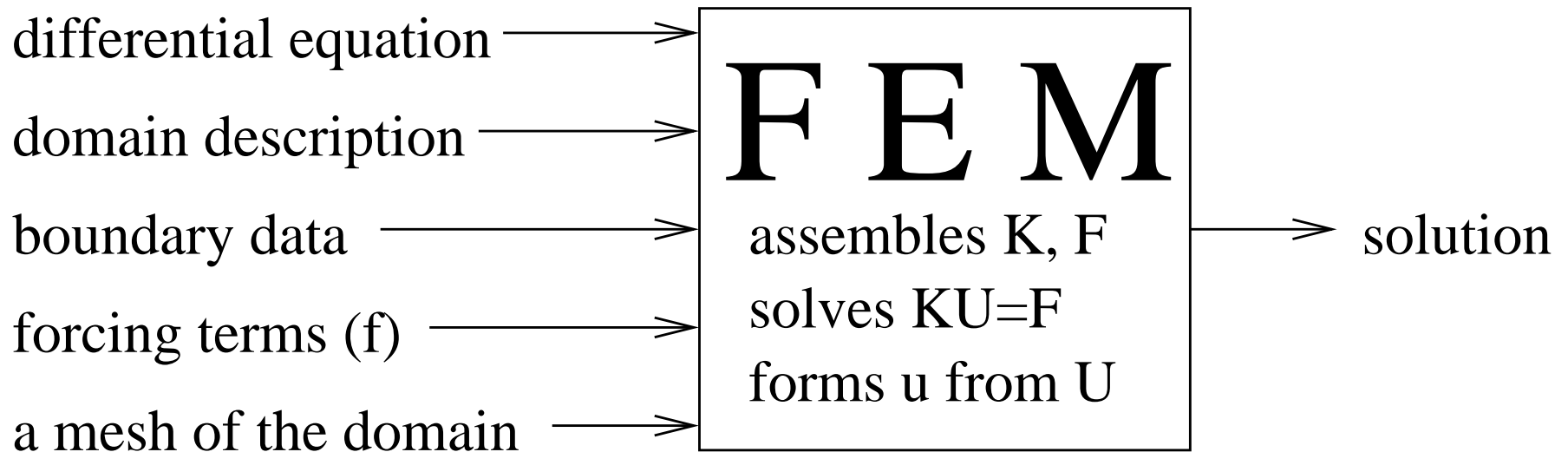


Figure 1: Black box into which one puts model problem and out of which pops an algorithm ( $KU = F$ ) for approximating the corresponding solutions.

## 1.1 Weak Formulation of Boundary Value Problems

Consider the two-point boundary value problem

$$\begin{aligned} -\frac{d^2u}{dx^2} &= f \text{ in } \Omega \\ u(0) &= 0, \quad u'(1) = 0. \end{aligned} \tag{1.1}$$

where  $\Omega = (0, 1)$ . Define a space incorporating the **essential boundary condition**:

$$V = \{v \in L^2(\Omega) : a(v, v) < \infty \text{ and } v(0) = 0\}.$$

(1) Multiply the differential equation in (1.1) by  $v \in V$ :

$$f(x)v(x) = -u''(x)v(x) \tag{1.2}$$

(2) Integrate (1.2) over the domain  $\Omega$ :

$$\int_0^1 f(x)v(x)dx = \int_0^1 -u''(x)v(x)dx \tag{1.3}$$

## Continuation of three-step recipe

(3) Integrate by parts (1.3) to get

$$\begin{aligned}(f, v) &:= \int_0^1 f(x)v(x)dx = \int_0^1 -u''(x)v(x)dx \\ &= \int_0^1 u'(x)v'(x)dx =: a(u, v).\end{aligned}\tag{1.4}$$

Then we can say that the solution  $u$  to (1.1) is characterized by

$$u \in V \quad \text{such that} \quad a(u, v) = (f, v) \quad \forall v \in V,\tag{1.5}$$

which is called the *variational* or *weak* formulation of (1.1).

**Theorem 1.1** *Suppose  $f \in C^0([0, 1])$  and  $u \in C^2([0, 1])$  satisfy (1.5). Then  $u$  solves (1.1).*

## 1.2 Naming conventions for two types of boundary conditions

Boundary Condition	Variational Name	Proper Name
$u(x) = 0$	essential	Dirichlet
$u'(x) = 0$	natural	Neumann

Table 1: Naming conventions for two types of boundary conditions.

The assumptions  $f \in C^0([0, 1])$  and  $u \in C^2([0, 1])$  in the theorem allow (1.1) to be interpreted in the usual sense.

But the variational problem can be solved with much more general  $f$ , including ones that are not functions, such as the Dirac  $\delta$ :

$$(\delta, f) = f(a)$$

for some  $a \in \Omega$ .

For this reason, (1.5) is also called a *weak* formulation of (1.1).

## 1.3 Ritz-Galerkin Approximation

Let  $S \subset V$  be any (finite dimensional) subspace. Let us consider (1.5) with  $V$  replaced by  $S$ , namely

$$u_S \in S \quad \text{such that} \quad a(u_S, v) = (f, v) \quad \forall v \in S. \quad (1.6)$$

**Theorem 1.2** *Given  $f \in L^2(0, 1)$ , (1.6) has a unique solution.*

Write (1.6) in terms of a basis of  $S$ :  $\{\phi_i : 1 \leq i \leq n\}$ , and expand

$$u_S = \sum_{j=1}^n U_j \phi_j$$

$$K_{ij} = a(\phi_j, \phi_i), F_i = (f, \phi_i) \quad \text{for} \quad i, j = 1, \dots, n.$$

Set  $\mathbf{U} = (U_j)$ ,  $\mathbf{K} = (K_{ij})$  and  $\mathbf{F} = (F_i)$ .

Then (1.6) is equivalent to solving the (square) matrix equation

$$\mathbf{KU} = \mathbf{F}. \quad (1.7)$$

For a square system such as (1.7) we know that uniqueness is equivalent to existence, as this is a *finite dimensional* system.

To prove uniqueness, we show that nonuniqueness implies a contradiction.

Nonuniqueness would imply that there is a nonzero  $\mathbf{V}$  such that  $\mathbf{KV} = \mathbf{0}$ .

For  $v = \sum V_j \phi_j$ , this means that  $0 = a(v, v) = \int_0^1 (v')^2(x) dx$ , from which we conclude that  $\mathbf{V} = \mathbf{0}$ .

Thus, the solution to (1.7) must be unique (and hence must exist).

Therefore, the solution  $u_S$  to (1.6) must also exist and be unique.

The matrix  $\mathbf{K}$  is often referred to as the *stiffness* matrix, a name coming from corresponding matrices in the context of structural problems.

It is symmetric, since the *energy* inner-product  $a(\cdot, \cdot)$  is symmetric.

It is also *positive definite*, since

$$\sum_{i,j=1}^n k_{ij} v_i v_j = a(v, v) \quad \text{where} \quad v = \sum_{j=1}^n v_j \phi_j.$$

## 1.4 Piecewise Polynomial Spaces – The Finite Element Method

Let  $0 = x_0 < x_1 < \dots < x_n = 1$  be a partition of  $[0, 1]$ , and let  $S$  be the linear space of functions generated by the basis functions shown in Fig. 2.

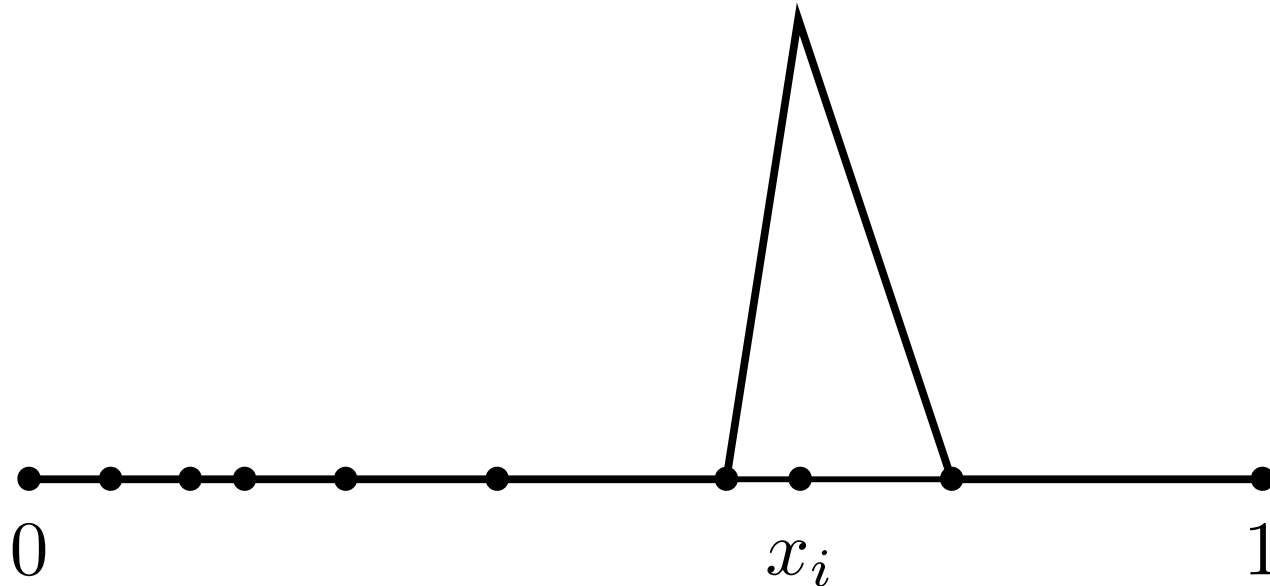


Figure 2: piecewise linear basis function  $\phi_i$

$\{\phi_i\}$  is called a **nodal** basis for  $S$ , and  $\{v(x_i)\}$  are the **nodal values** of a function  $v$ . (The points  $\{x_i\}$  are called the **nodes**.)

## 1.5 Computer Implementation of Finite Element Methods

The key step in this process is the *assembly* of the inner-product  $a(u, v)$  by summing its constituent parts over each sub-interval, or *element*, which are computed separately.

This is facilitated through the use of a numbering scheme called the *local-to-global* index.

This index,  $i(e, j)$ , relates the local node number,  $j$ , on a particular element,  $e$ , to its position in the global data structure.

In our one-dimensional example with piecewise linear functions, this index is particularly simple: the “elements” are based on the intervals  $I_e := [x_{e-1}, x_e]$  where  $e$  is an integer in the range  $1, \dots, n$  and

$$i(e, j) := e + j - 1 \text{ for } e = 1, \dots, n \text{ and } j = 0, 1.$$

That is, for each element there are two nodal parameters of interest, one corresponding to the left end of the interval ( $j = 0$ ) and one at the right ( $j = 1$ ). Their relationship is represented by the mapping  $i(e, j)$ .



We may write the interpolant of a continuous function  $f$  or of a vector  $F$  as

$$f_I := \sum_e \sum_{j=0}^1 f_{i(e,j)} \phi_j^e := \sum_e \sum_{j=0}^1 f(x_{i(e,j)}) \phi_j^e$$

where  $\{\phi_j^e \ni j = 0, 1\}$  denotes the set of basis functions for linear functions on the single interval  $I_e = [x_{e-1}, x_e]$ :

$$\phi_j^e(x) = \phi_j((x - x_{e-1}) / (x_e - x_{e-1}))$$

where

$$\phi_0(x) := \begin{cases} 1 - x & x \in [0, 1] \\ 0 & \textit{otherwise} \end{cases}$$

and

$$\phi_1(x) := \begin{cases} x & x \in [0, 1] \\ 0 & \textit{otherwise.} \end{cases}$$

Note that we have related all of the “local” basis functions  $\phi_j^e$  to a fixed set of basis functions on a “reference” element,  $[0, 1]$ , via an affine mapping of  $[0, 1]$  to  $[x_{e-1}, x_e]$ . (By definition, the local basis functions,  $\phi_j^e$ , are extended by zero outside the interval  $I_e$ .)

The bilinear forms defined in (1.4) can be assembled using this representation:

$$a(v, w) = \sum_e a_e(v, w)$$

where the “local” bilinear form is defined (and evaluated) via

$$\begin{aligned} a_e(v, w) &:= \int_{I_e} v' w' dx \\ &= (x_e - x_{e-1})^{-1} \begin{pmatrix} v_{i(e,0)} \\ v_{i(e,1)} \end{pmatrix}^t \mathbf{K} \begin{pmatrix} w_{i(e,0)} \\ w_{i(e,1)} \end{pmatrix}. \end{aligned} \quad (1.8)$$

Here, the *local stiffness matrix*,  $\mathbf{K}$ , is given by

$$\mathbf{K}_{i,j} := \int_0^1 \phi'_{i-1} \phi'_{j-1} dx \text{ for } i, j = 1, 2.$$

## 1.6 More weak formulations

Consider the two-point boundary value problem

$$\begin{aligned} -\frac{d^2u}{dx^2} + \lambda u &= f \text{ in } \Omega \\ u(0) &= 0, \quad u'(1) = 0. \end{aligned} \tag{1.9}$$

where  $\Omega = (0, 1)$ . Define

$$V = \{v \in L^2(\Omega) : a(v, v) < \infty \text{ and } v(0) = 0\}.$$

- (1) Multiply the differential equation in (1.9) by  $v \in V$ ,
- (2) Integrate over the domain  $\Omega$ , and (3) Integrate by parts to get

$$(f, v) = \int_0^1 u'(x)v'(x) + \lambda v(x)u(x)dx =: a(u, v). \tag{1.10}$$

This leads to  $KU + \lambda MU = F$ , where  $M$  is called the mass matrix:  $M_{ij} = (\phi_i, \phi_j)$ . This equation will be **singular for some  $\lambda < 0$**  since it corresponds to an eigenvalue problem:  $M^{-1}KU = -\lambda U$ .

## 1.7 Different boundary conditions

Consider the boundary conditions

$$\begin{aligned}u(0) &= 0, & u(1) &= 0 \\u(0) &= 0, & u'(1) &= 0 \\u'(0) &= 0, & u(1) &= 0 \\u'(0) &= 0, & u'(1) &= 0\end{aligned}\tag{1.11}$$

These correspond to the spaces

$$\begin{aligned}V &= \{v \in W : v(0) = 0 \text{ and } v(1) = 0\} \\V &= \{v \in W : v(0) = 0\} \\V &= \{v \in W : v(1) = 0\} \\V &= W\end{aligned}\tag{1.12}$$

respectively, where  $W$  is the space

$$W = \{v \in L^2(\Omega) : a(v, v) < \infty\}$$

## 1.8 Multiple weak formulations

Consider the two-point boundary value problem

$$-\frac{d^2u}{dx^2} + \frac{du}{dx} = f \text{ in } \Omega \quad (1.13)$$

where  $\Omega = (0, 1)$ . This leads to multiple variational formulations:

$$\begin{aligned} \int_0^1 u'(x)v'(x) + v(x)u'(x)dx &=: a_1(u, v). \\ \int_0^1 u'(x)v'(x) - v'(x)u(x)dx &=: a_2(u, v). \end{aligned} \quad (1.14)$$

depending on whether or not we integrate by parts on the second term on the left hand side in (1.13)

For this reason, using variational forms as a language avoids some ambiguity in the model definition.

## 2 Matrix Evaluation by Assembly

The *assembly* of integrated differential forms is done by summing its constituent parts over each *element*, which are computed separately through the use of a numbering scheme called the *local-to-global* index. This index,  $\iota(e, \lambda)$ , relates the local (or element) node number,  $\lambda \in \mathcal{L}$ , on a particular element, indexed by  $e$ , to its position in the global data structure.

We may write a finite element function  $f$  in the form

$$\sum_e \sum_{\lambda \in \mathcal{L}} f_{\iota(e, \lambda)} \phi_\lambda^e \quad (2.15)$$

where  $f_i$  denotes the “nodal value” of the finite element function at the  $i$ -th node in the global numbering scheme and  $\{\phi_\lambda^e \ni \lambda \in \mathcal{L}\}$  denotes the set of basis functions on the element domain  $T_e$ .

The element basis functions,  $\phi_\lambda^e$ , are extended by zero outside  $T_e$ .

Can relate “element” basis functions  $\phi_\lambda^e$  to fixed set of basis functions on “reference” element,  $\mathcal{T}$ , via mapping of  $\mathcal{T}$  to  $T_e$ .

Could involve changing both the “ $x$ ” values and the “ $\phi$ ” values in a coordinated way, as with the Piola transform, or it could be one whose Jacobian is non-constant, as with tensor-product elements or isoparametric elements.

For an affine mapping,  $\xi \rightarrow J\xi + x_e$ , of  $\mathcal{T}$  to  $T_e$ :

$$\phi_\lambda^e(x) = \phi_\lambda(J^{-1}(x - x_e)).$$

The inverse mapping,  $x \rightarrow \xi = J^{-1}(x - x_e)$  has as its Jacobian

$$J_{mj}^{-1} = \frac{\partial \xi_m}{\partial x_j},$$

and this is the quantity which appears in the evaluation of the bilinear forms. Of course,  $\det J = 1 / \det J^{-1}$ .

## 2.1 Evaluation of bilinear forms

The assembly algorithm utilizes the decomposition of a variational form as a sum over “element” forms

$$a(v, w) = \sum_e a_e(v, w)$$

where “element” bilinear form for Laplace’s equation defined via

$$\begin{aligned} a_e(v, w) &:= \int_{T_e} \nabla v(x) \cdot \nabla w(x) dx \\ &= \int_T \sum_{j=1}^d \frac{\partial}{\partial x_j} v(J\xi + x_e) \frac{\partial}{\partial x_j} w(J\xi + x_e) \det(J) d\xi \end{aligned} \tag{2.16}$$

by transforming to the reference element.

Finite element matrices computed via assembly in a similar way.

The local element form is computed as follows.



## 2.2 Evaluation of bilinear forms—continued

$$\begin{aligned}
 a_e(v, w) &= \int_{\mathcal{T}} \sum_{j=1}^d \frac{\partial}{\partial x_j} v(J\xi + x_e) \frac{\partial}{\partial x_j} w(J\xi + x_e) \det(J) d\xi \\
 &= \int_{\mathcal{T}} \sum_{j,m,m'=1}^d \frac{\partial \xi_m}{\partial x_j} \frac{\partial}{\partial \xi_m} \left( \sum_{\lambda \in \mathcal{L}} v_{\iota(e,\lambda)} \phi_{\lambda}(\xi) \right) \times \\
 &\quad \frac{\partial \xi_{m'}}{\partial x_j} \frac{\partial}{\partial \xi_{m'}} \left( \sum_{\mu \in \mathcal{L}} w_{\iota(e,\mu)} \phi_{\mu}(\xi) \right) \det(J) d\xi \quad (2.17) \\
 &= \begin{pmatrix} v_{\iota(e,1)} \\ \cdot \\ \cdot \\ v_{\iota(e,|\mathcal{L}|)} \end{pmatrix}^t \mathbf{K}^e \begin{pmatrix} w_{\iota(e,1)} \\ \cdot \\ \cdot \\ w_{\iota(e,|\mathcal{L}|)} \end{pmatrix}.
 \end{aligned}$$

Here, the *element stiffness matrix*,  $\mathbf{K}^e$ , is given by

$$\begin{aligned}
 K_{\lambda,\mu}^e &:= \sum_{j,m,m'=1}^d \frac{\partial \xi_m}{\partial x_j} \frac{\partial \xi_{m'}}{\partial x_j} \det(J) \int_{\mathcal{T}} \frac{\partial}{\partial \xi_m} \phi_\lambda(\xi) \frac{\partial}{\partial \xi_{m'}} \phi_\mu(\xi) d\xi \\
 &= \sum_{m,m'=1}^d G_{m,m'}^e K_{\lambda,\mu,m,m'}
 \end{aligned} \tag{2.18}$$

where

$$K_{\lambda,\mu,m,m'} = \int_{\mathcal{T}} \frac{\partial}{\partial \xi_m} \phi_\lambda(\xi) \frac{\partial}{\partial \xi_{m'}} \phi_\mu(\xi) d\xi \tag{2.19}$$

and

$$G_{m,m'}^e := \det(J) \sum_{j=1}^d \frac{\partial \xi_m}{\partial x_j} \frac{\partial \xi_{m'}}{\partial x_j} \tag{2.20}$$

for  $\lambda, \mu \in \mathcal{L}$  and  $m, m' = 1, \dots, d$ .

### 3 Revue of Adaptivity

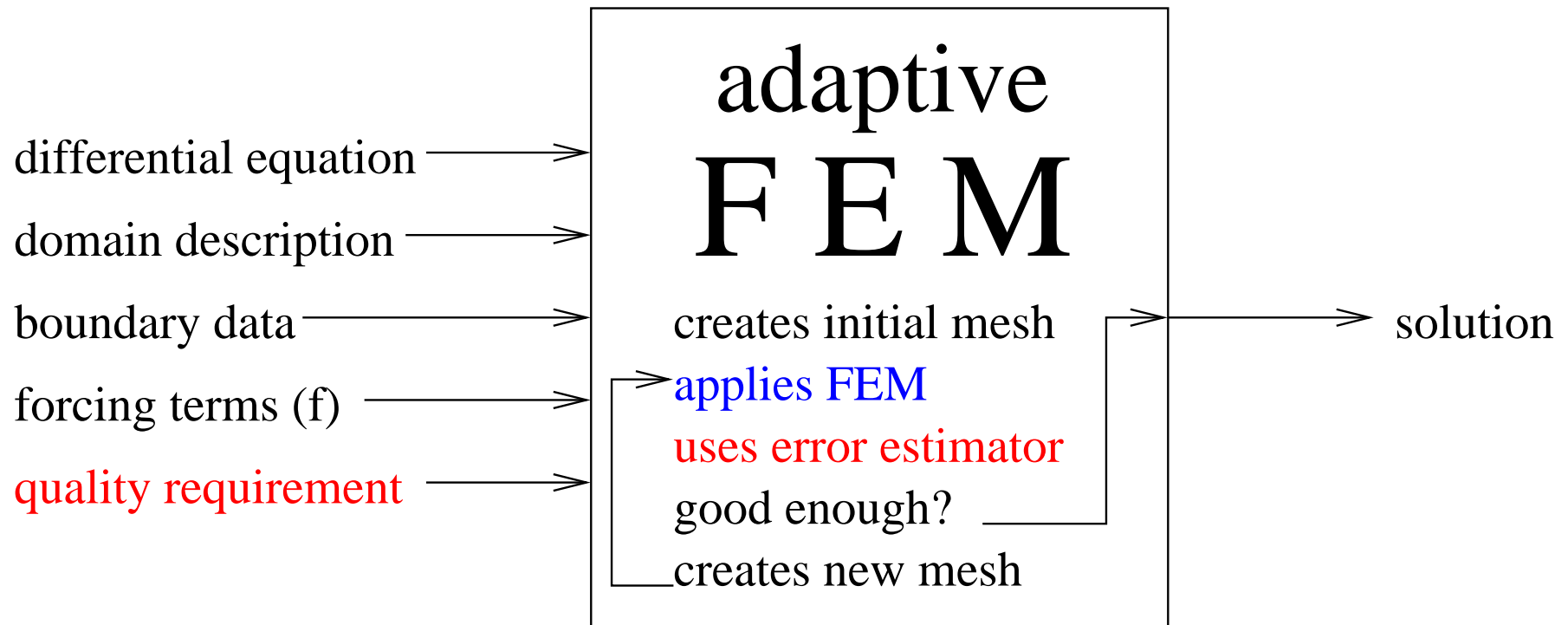


Figure 3: Black box for adaptive FEM; requires no mesh initially, only quality requirement. Generates a sequence of meshes and applies standard FEM until quality is assured.

## Model problem

We consider a variational problem with “energy” form

$$a(v, w) = \int_{\Omega} \alpha(x) \nabla v \cdot \nabla w \, dx \quad (3.21)$$

Solve for  $u_h \in V_h$  such that

$$a(u_h, v) = (f, v) \quad \forall v \in V_h \quad (3.22)$$

The error  $e_h := u - u_h$  satisfies the *residual equation*

$$a(e_h, v) = R(v) \quad \forall v \in V \quad (3.23)$$

where the *residual*  $R \in V'$  is defined by  $R(v) :=$

$$\sum_T \int_T (f - \nabla \alpha \cdot \nabla u_h) v \, dx + \sum_e \int_e [\alpha \mathbf{n} \cdot \nabla u_h] v \, ds \quad (3.24)$$

If  $\mathcal{A}$  is the differential operator associated with the form (3.21), namely,  $\mathcal{A}v := -\nabla \cdot (\alpha \nabla v)$ , then we see that  $R_A = \mathcal{A}(u - u_h) = \mathcal{A}e_h$  on each  $T$ .

Relations (3.23–3.24) can be derived automatically.

The *local error indicator*  $\mathcal{E}_e$  by

$$\begin{aligned} \mathcal{E}_e(u_h)^2 := & \sum_{T \subset T_e} h_T^2 \|f - \nabla \alpha \cdot \nabla u_h\|_{L^2(T)}^2 \\ & + h_e \| [\alpha \mathbf{n} \cdot \nabla u_h] \|_{L^2(e)}^2 \end{aligned} \quad (3.25)$$

can also be generated automatically from the description (3.21).

With this definition, we showed that

$$|e_h|_{H^1(\Omega)} \leq \frac{\gamma}{\alpha_0} \left( \sum_e \mathcal{E}_e(u_h)^2 \right)^{1/2} \quad (3.26)$$

where  $\gamma$  is only related to interpolation error.

From the error estimate, a better mesh can be determined: we refine where  $\mathcal{E}_e(u_h)$  is large.

The process is repeated to get a more accurate simulation.

The use of adaptivity is more complicated but makes the simulation process much more efficient.

**But it all can be done automatically.**